# An Investigation on the Geometric Effects of a Vertical-Downward Elbow on Two-Phase Flow

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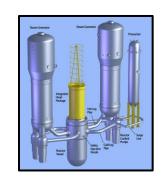
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Generously sponsored by the Toshiba-Westinghouse Fellows Program

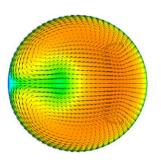
### This presentation investigates the geometric effects of a vertical-downward elbow on two-phase flow.



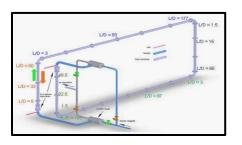
**Background** 



**Objective** 

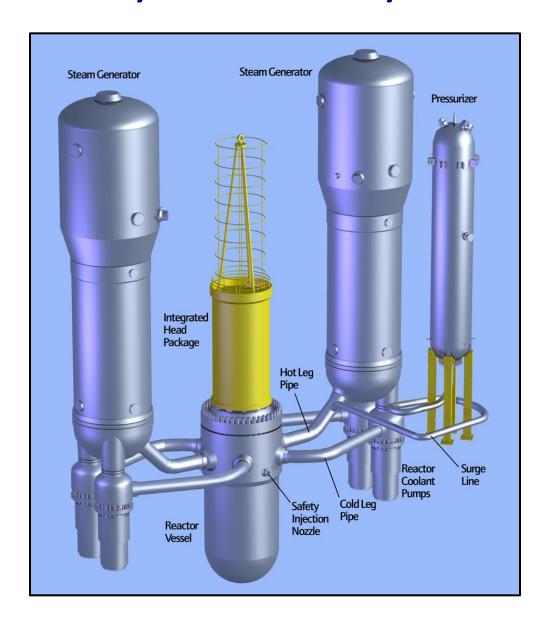


Single-Phase Flow CFD Modeling

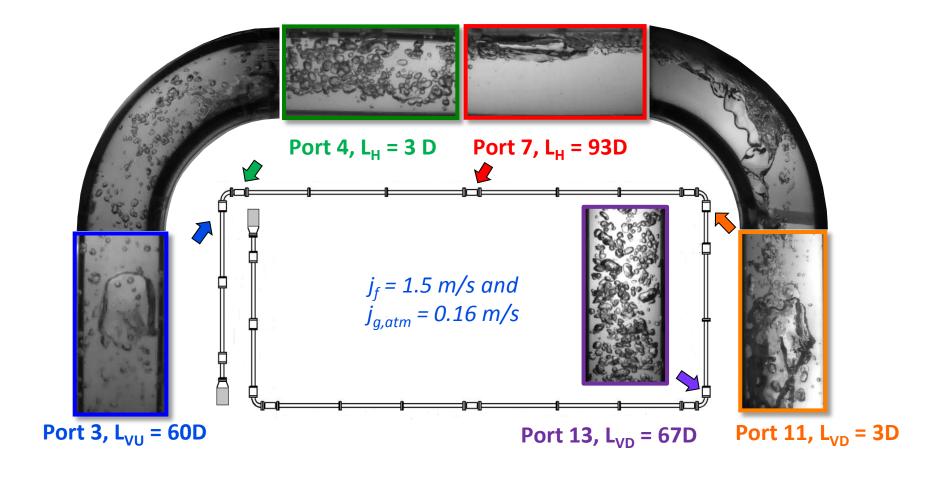


Two-Phase Flow Investigation

Researching geometric effects on two-phase flow can improve the safety of thermal-hydraulic reactor systems.



### Geometry and pipe orientation dramatically affect two-phase flow.



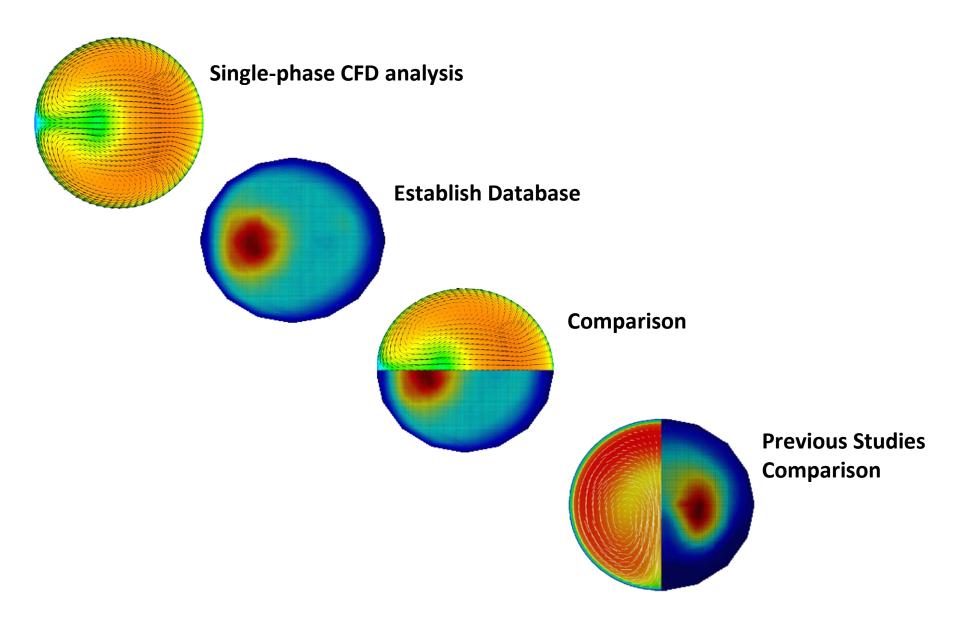
The experimental facility at Penn State enables data collection for a vertical-downward elbow. Vertical-**Downward** Width≅ 29.5 ft. **Elbow** Height≅ 10 ft. Water **Test Section** Flow Direction Elbow Radius = 6 in. Pipe Diameter = 2 in. The experimental facility at Penn State enables data collection for a vertical-downward elbow.



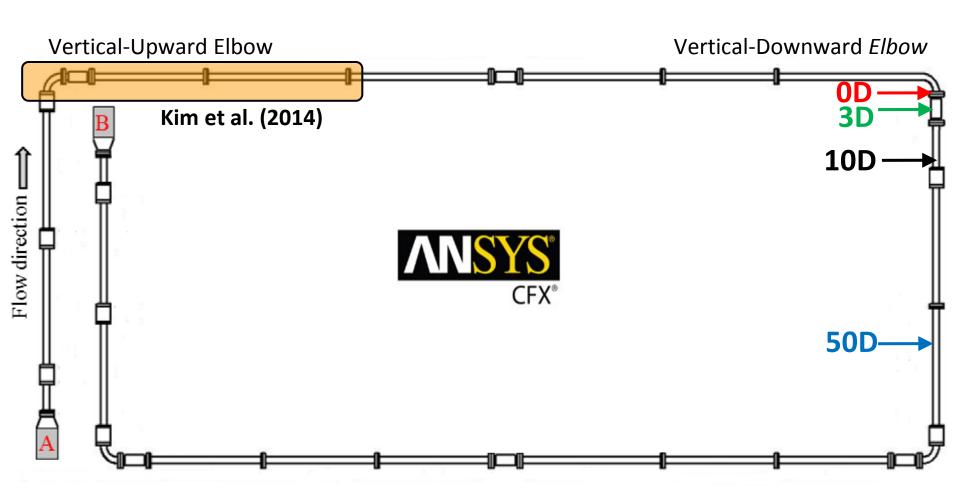
**Combinatorial Test Facility** 

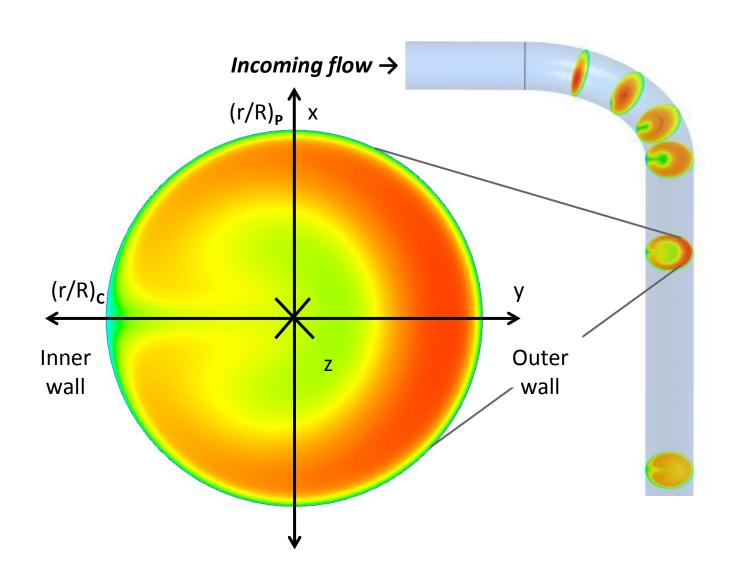
**Vertical-Downward Elbow** 

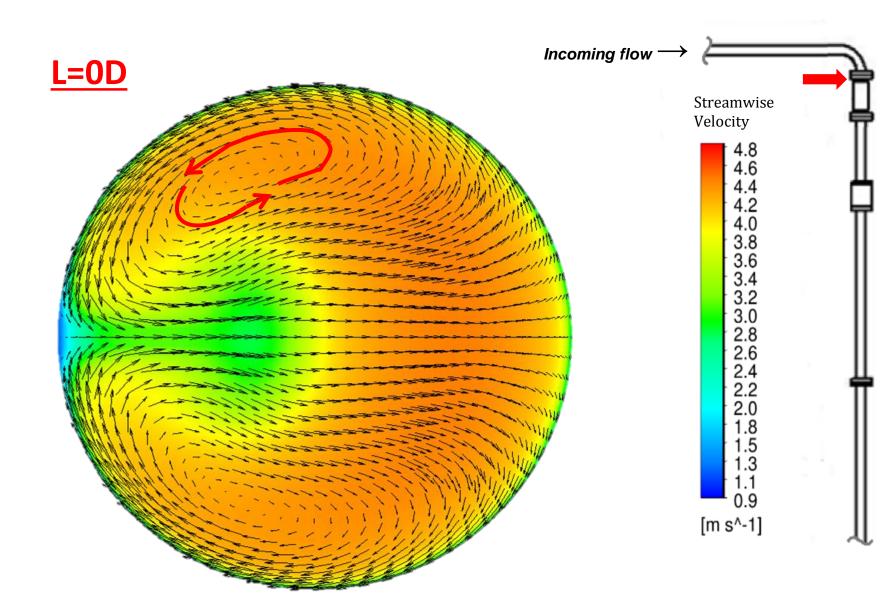
# The objective of this research is to investigate the impacts of a vertical-downward elbow.

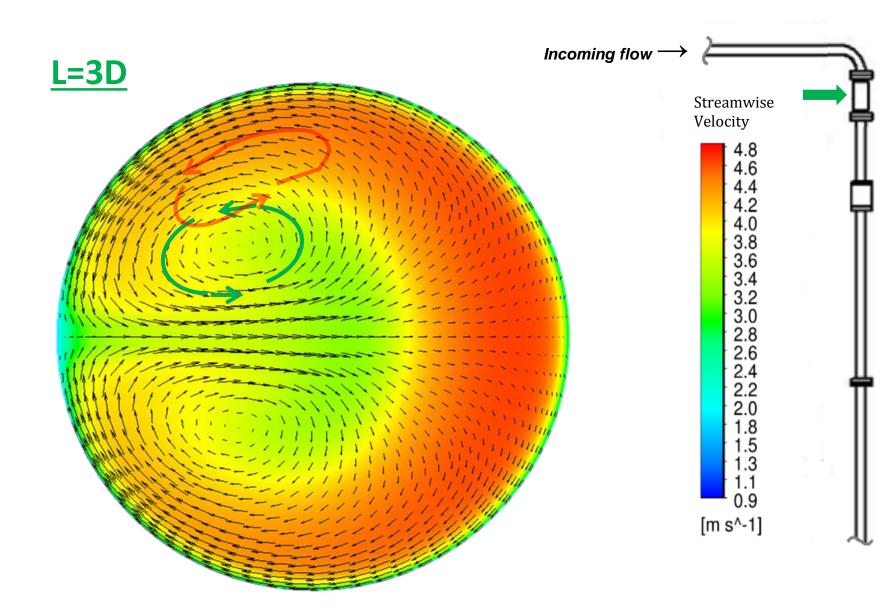


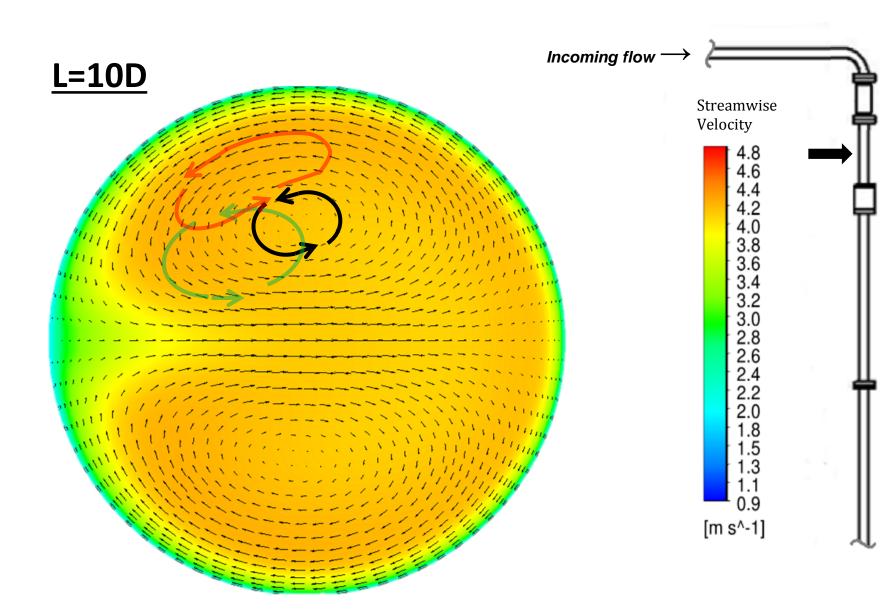
Single-phase flow in the facility was modeled with CFD to better understand the general elbow effects.

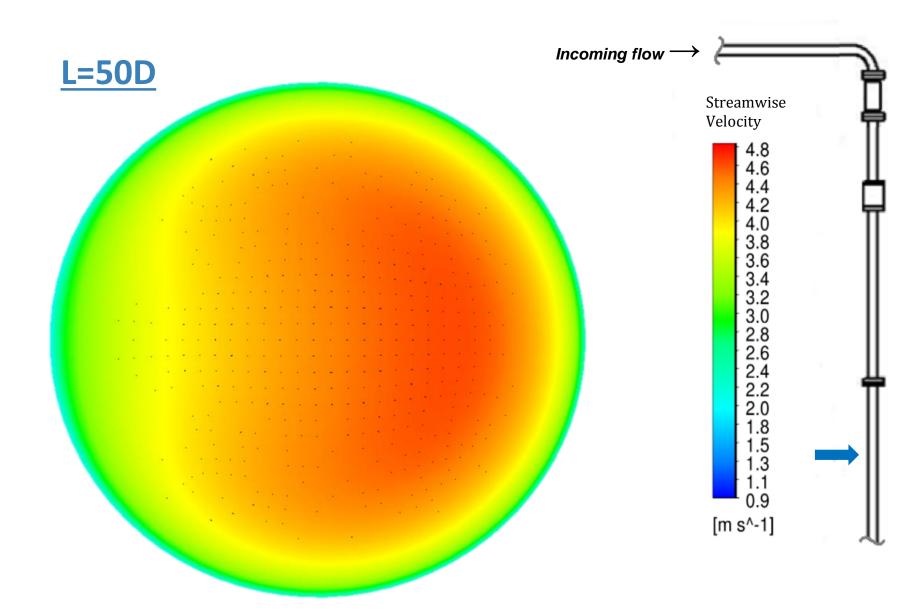


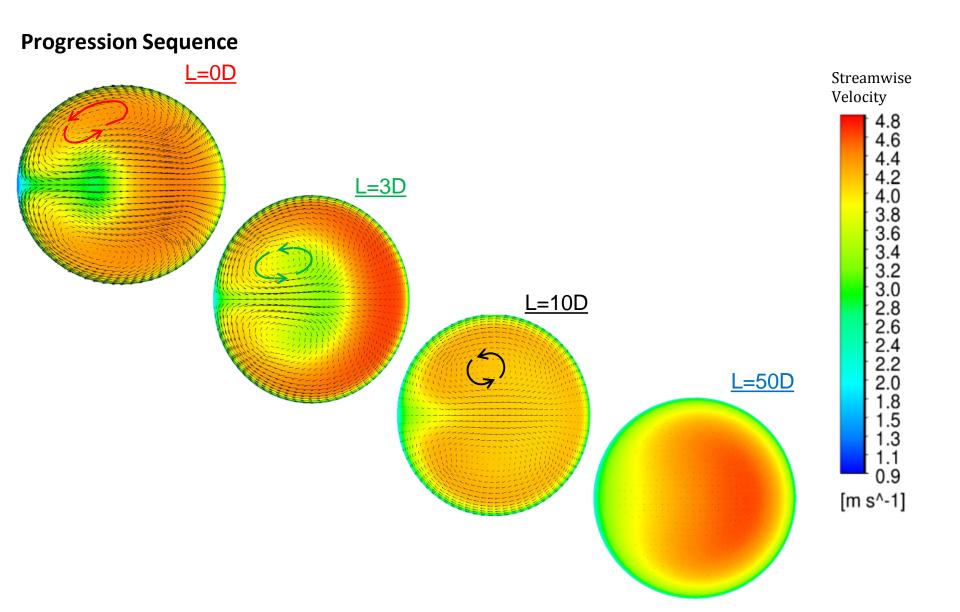




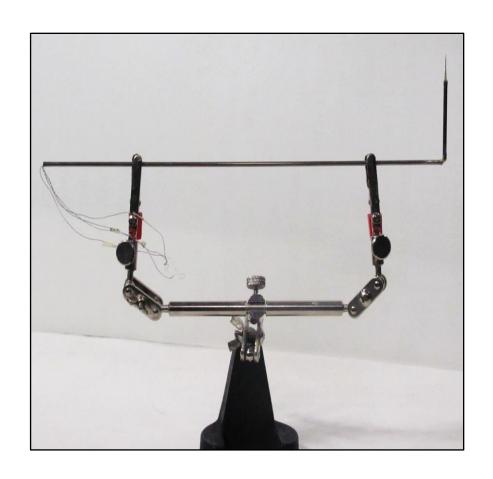


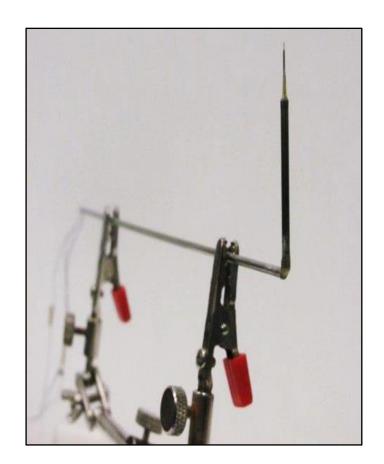






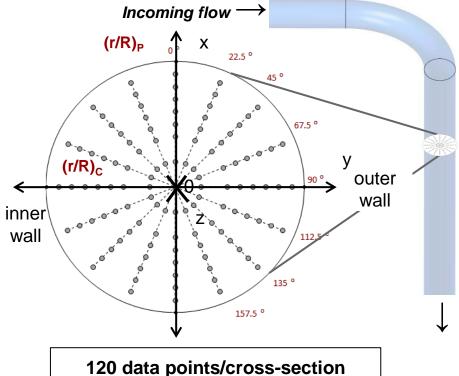
A four-sensor conductivity probe collects local data as it moves across the pipe with a specialized measurement port.



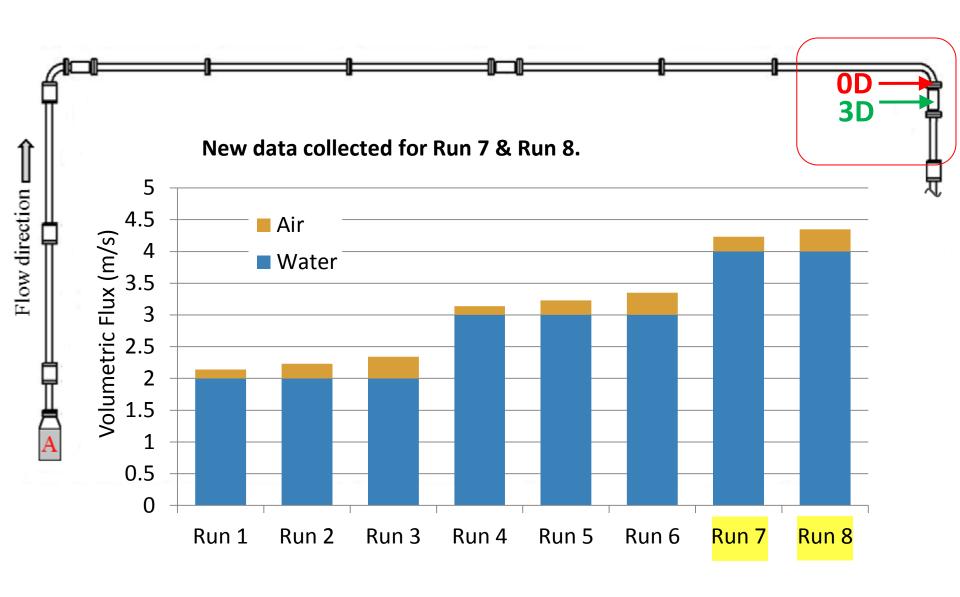


## A four-sensor conductivity probe collects local data as it moves across the pipe with a specialized measurement port.

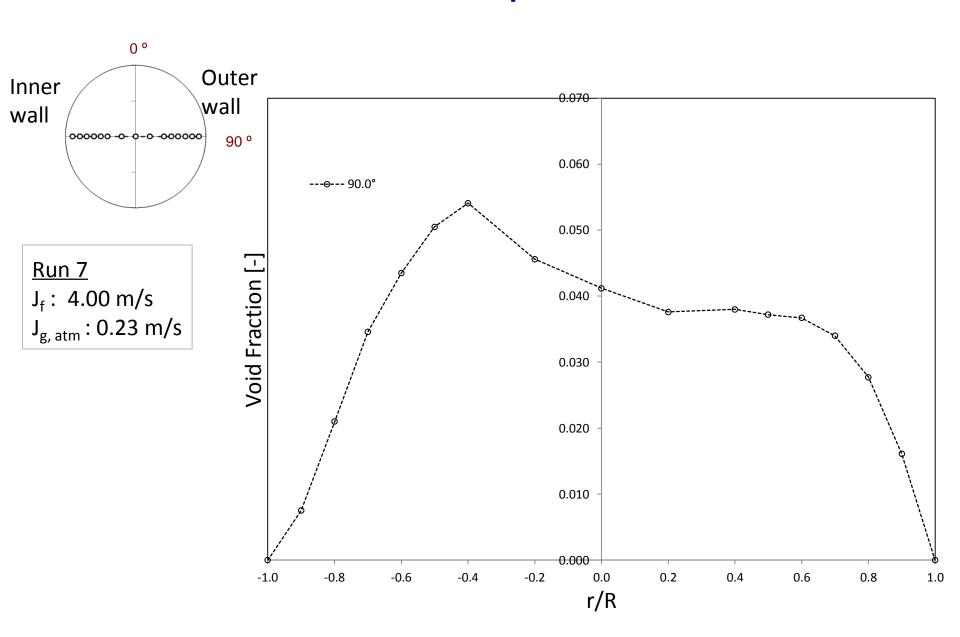




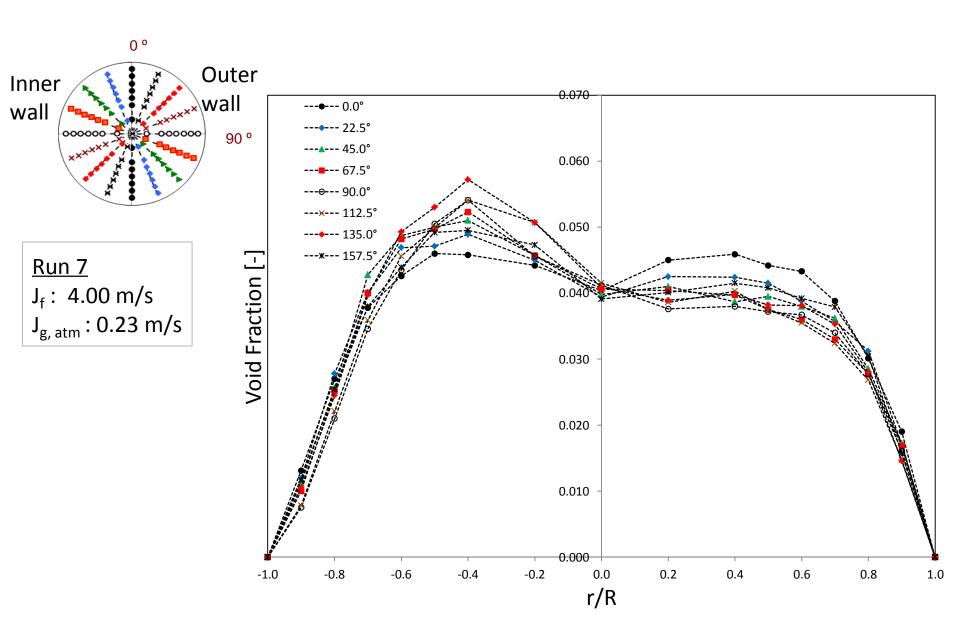
# New experimental data was collected at 0D and 3D after the vertical-downward elbow.



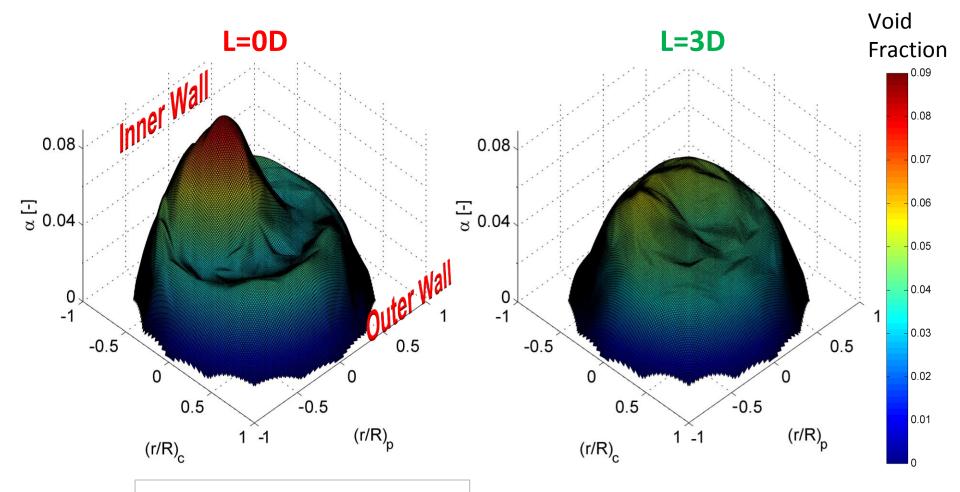
# Void fraction is measured with the conductivity probe in order to better understand two-phase flow structure.



# Void fraction is measured with the conductivity probe in order to better understand two-phase flow structure.

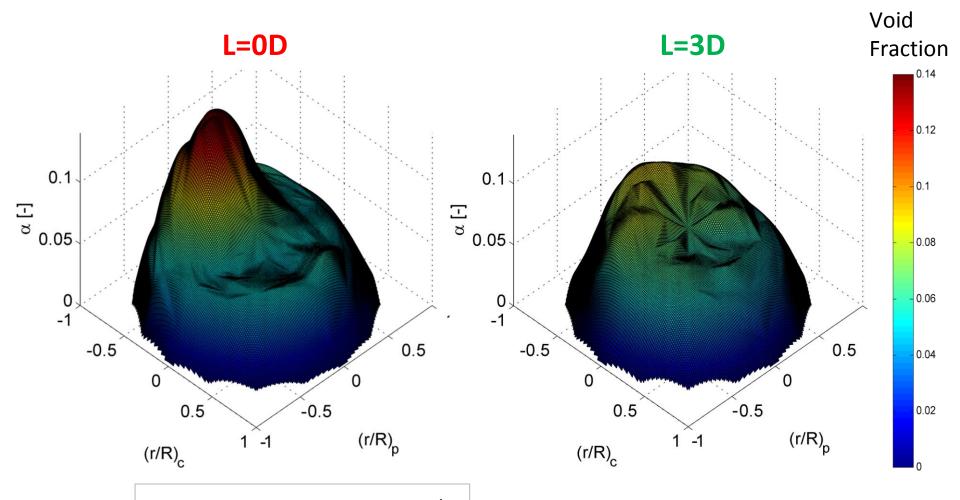


### The void fraction distribution reveals a single peak after the vertical-downward elbow.



**Run 7** Volumetric liquid flux: 4.00 m/s Volumetric gas flux: 0.23 m/s

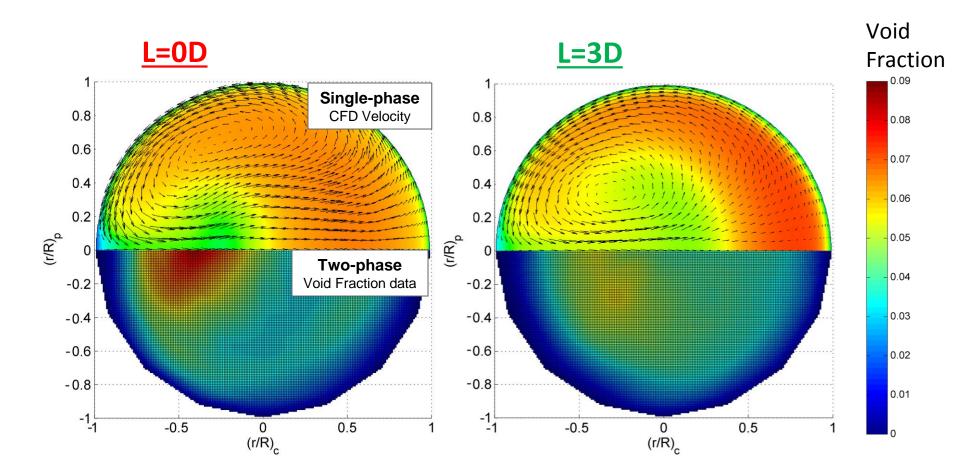
### The void fraction distribution reveals a single peak after the vertical-downward elbow.



Run 8

Volumetric liquid flux: 4.00 m/s Volumetric gas flux: 0.35 m/s

When compared, void fraction distribution and secondary flow show different flow characteristics.

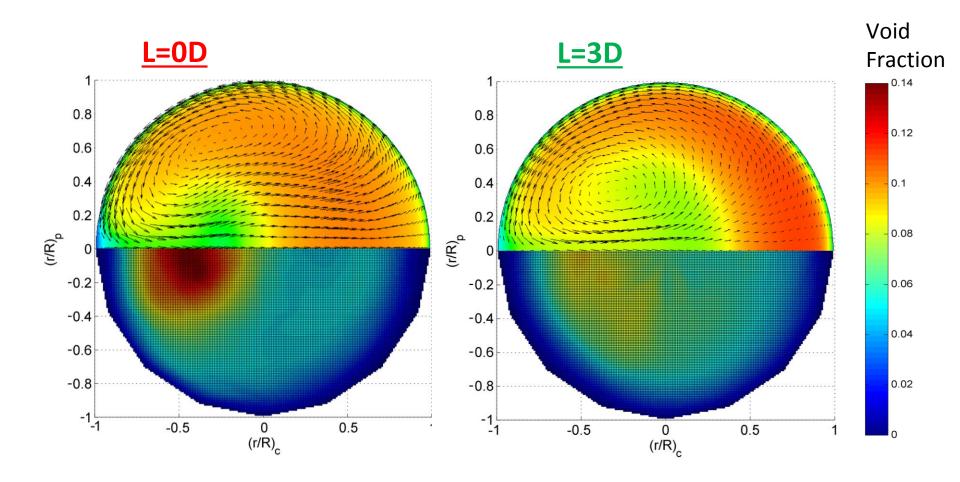


Run 7

Volumetric liquid flux: 4.00 m/s

Volumetric gas flux: 0.23 m/s

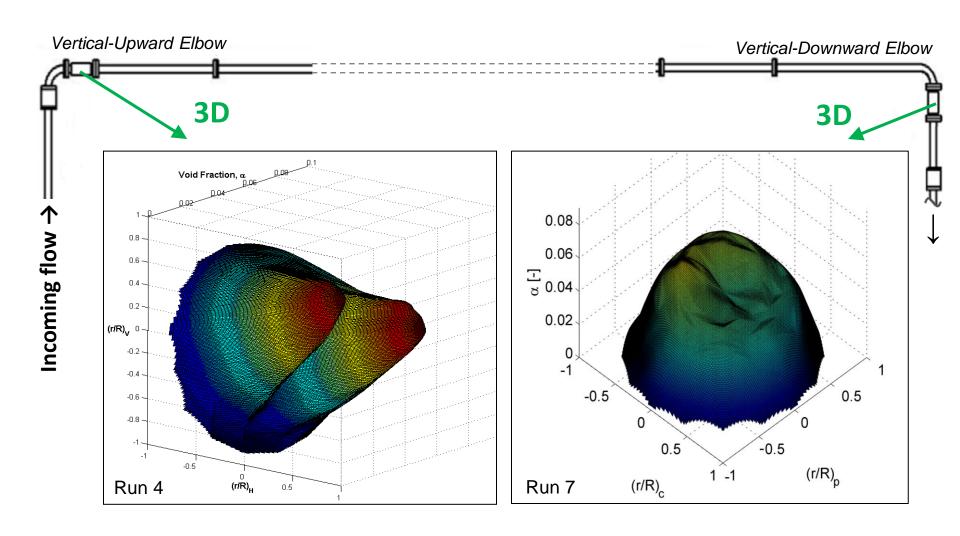
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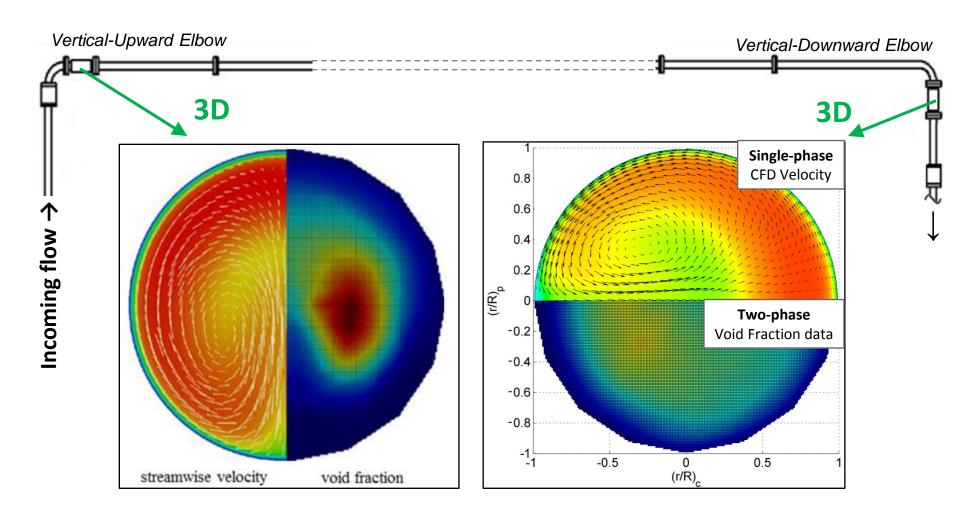
Run 8

Volumetric liquid flux: 4.00 m/s Volumetric gas flux: 0.35 m/s

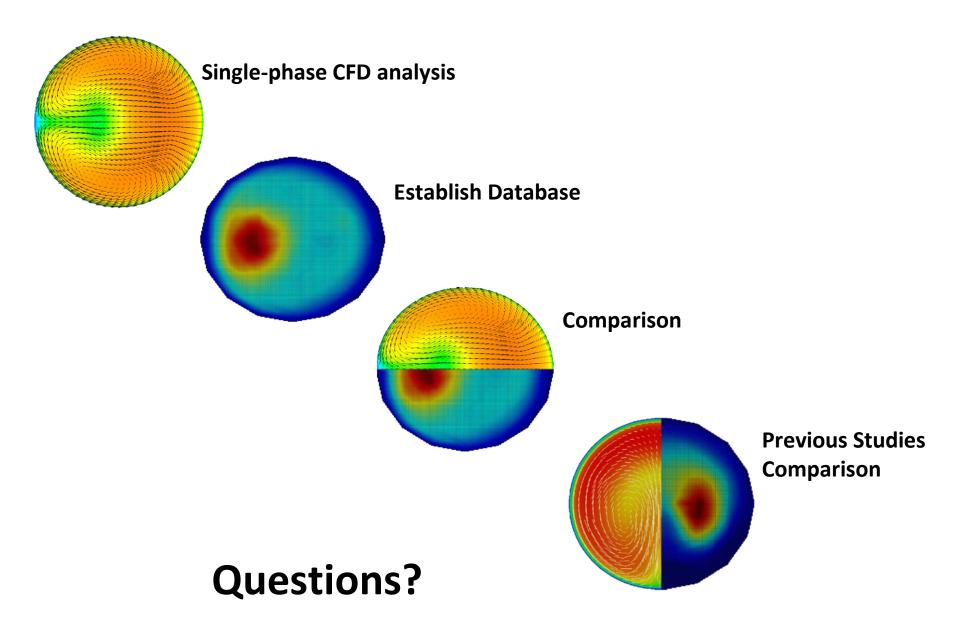
# Swirling has a different impact after the vertical-downward elbow in comparison to the vertical-upward elbow.



# Swirling has a different impact after the vertical-downward elbow in comparison to the vertical-upward elbow.



Our reasearch provides new data and results for the verticaldownward elbow for future reactor safety.



#### **ADDITIONAL SLIDES**



#### **Acknowledgements**

#### Special thanks to **Toshiba Westinghouse** for generously funding this Undergraduate Fellows Program.

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**Questions?** 

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Ph. D. Student The Pennsylvania State University szq105@psu.edu

#### **Recommendations for future work**

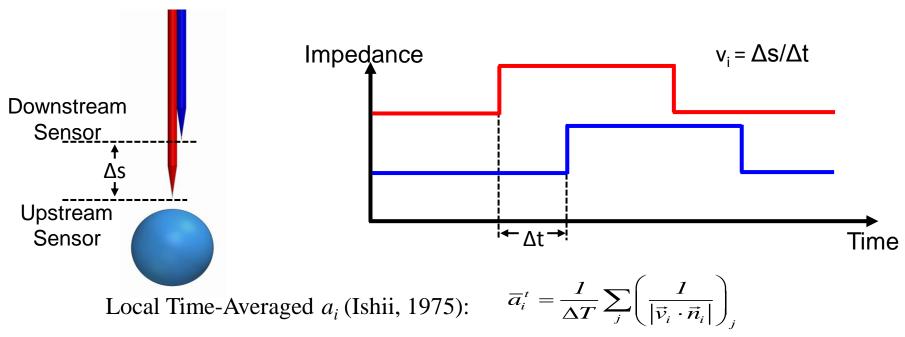
- Obtain more data for database of different flow rates and locations.
- Develop predictive models for two-phase flow around restrictions.
- Implement new models to reactor system analysis code for higher safety.

#### References

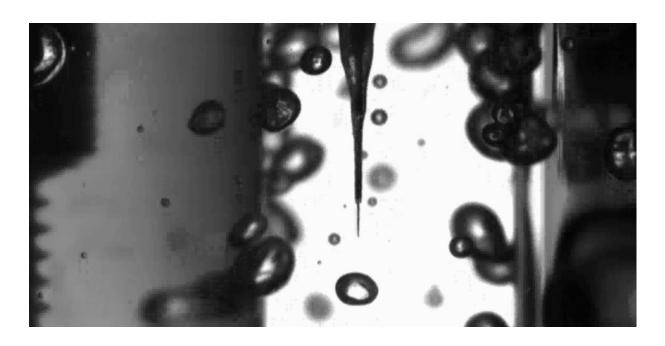
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### This slide shows the measurement principle of the four-sensor conductivity probe.

 Measurement principle: conductivity difference between gas and liquid phases

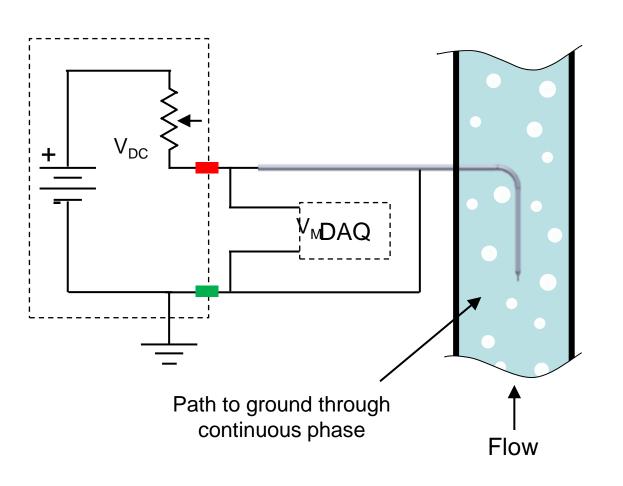


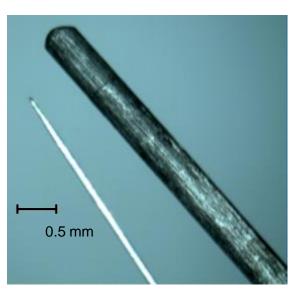
#### The state-of-the-art four-sensory conductivity probe creates minimal distortion of bubbles.



4000 fps

# These images show the size and configuration of the four-sensor conductivity probe.



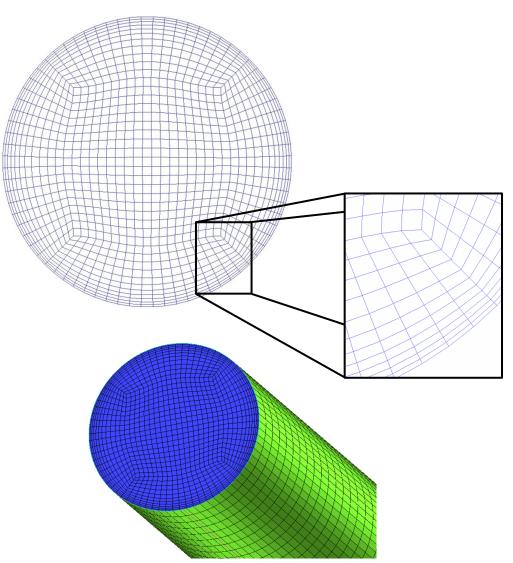


Acupuncture needle and 0.5 mm pencil lead

A mesh was generated for the loop geometry; this mesh was used as an input to the CFD solver.

Accurate solutions require a well-constructed mesh.

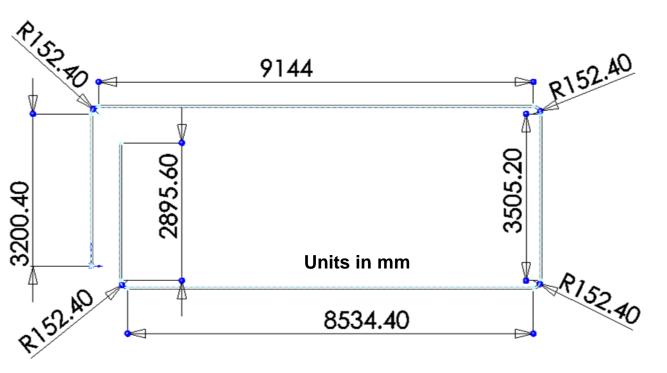
A mesh-sensitivity test confirmed that our results are grid-independent.

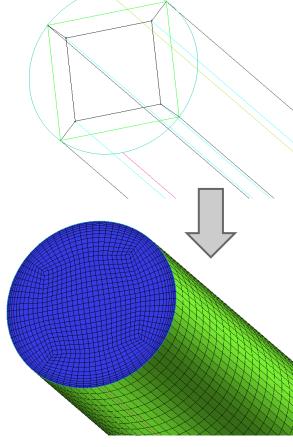


#### We have created high quality mesh to ensure accurate modeling

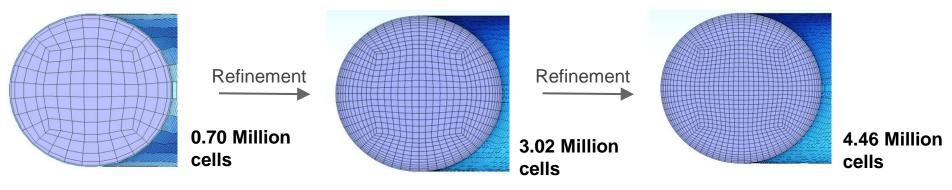
#### **Structured O-mesh**

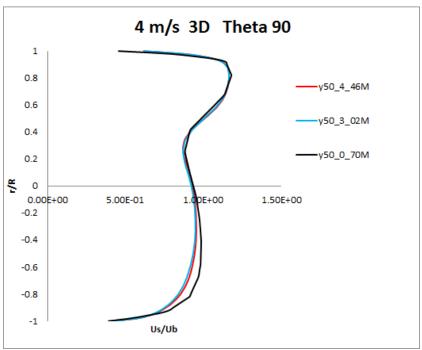
#### **Geometry accurately** represents the test facility

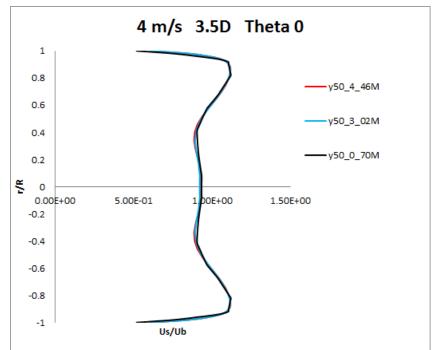




#### A mesh-sensitivity test demonstrates that our solution is gridindependent.







## The solution methods for our research compare well with previous research.

Kim, J., Yadav, M., & Kim, S. (2014). Characteristics of secondary flow induced by 90-degree elbow in turbulent pipe flow.

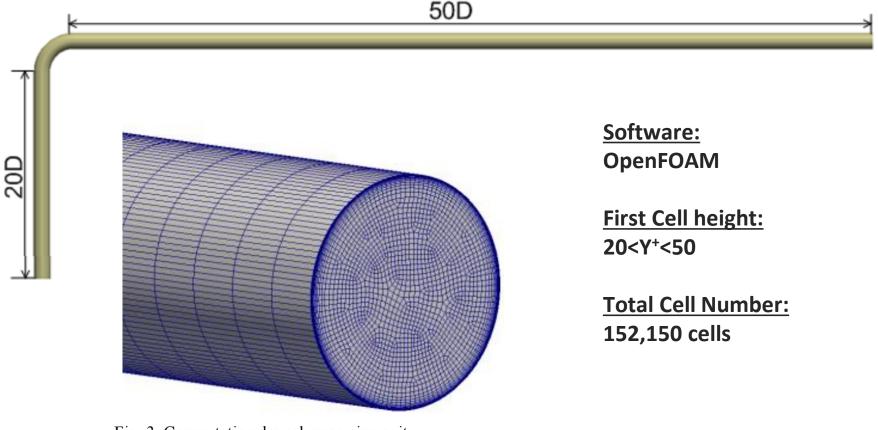
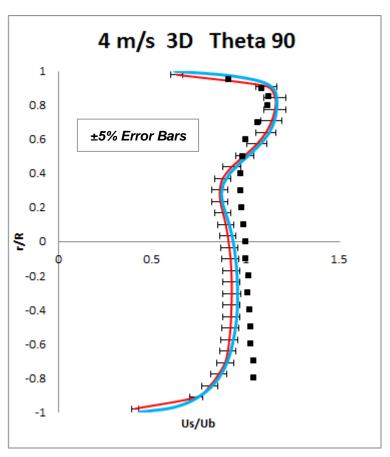
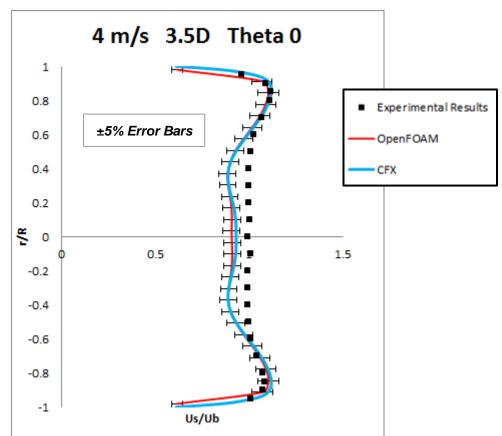


Fig. 3 Computational mesh near pipe exit.

# Our results for the vertical-upward elbow were compared with previous research to confirm the accuracy of our simulations.





## Secondary flow induced by elbow is seen to dissipate across nondimensional length through Swirl Intensity.

Swirl Intensity (I<sub>s</sub>) is defined as:

$$I_{s} = \frac{\int \left[\vec{U} - (\vec{U} \cdot \hat{n})\hat{n}\right]^{2} dA}{U_{b}^{2} \int dA}$$

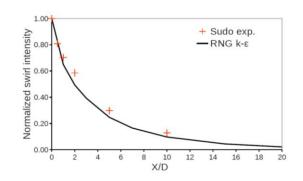


Fig. 17 Decay of swirl intensity along straight pipe after elbow with Rc = 2D.

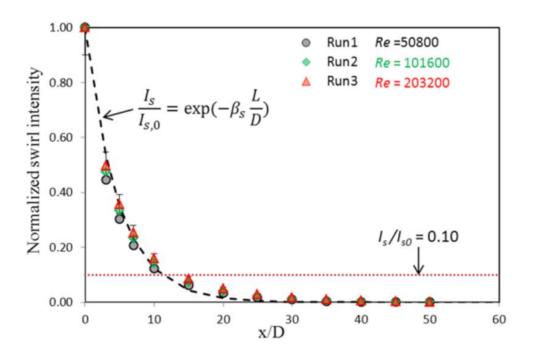


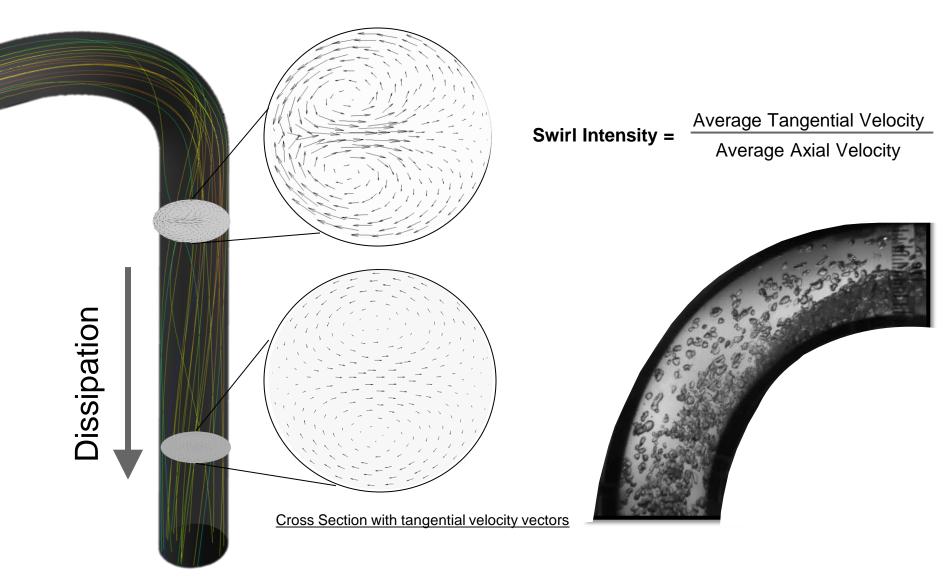
Fig. 18 Decay of normalized swirl intensity along pipe after elbow with Rc = 3D.

Kim et al. (2014) correlation:

$$\frac{I_s}{I_{s0}} = \exp(-\beta_s \frac{L}{D})$$

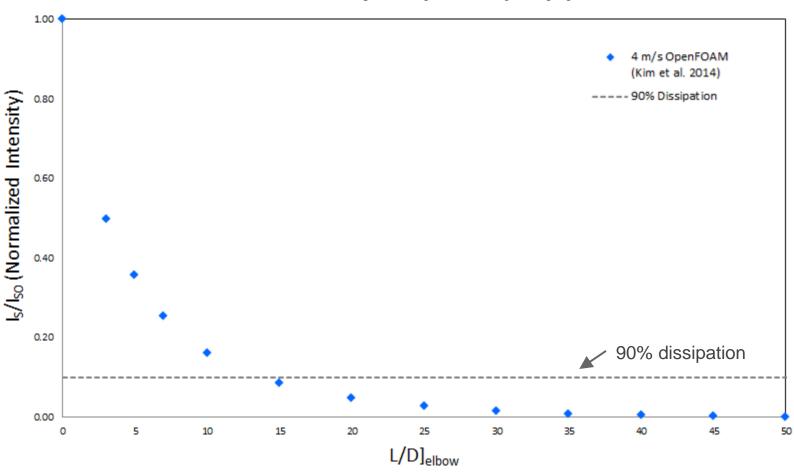
where  $\beta$ =0.21

# Swirl Intensity measures the magnitude of secondary flow, which dissipates after an elbow.

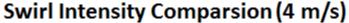


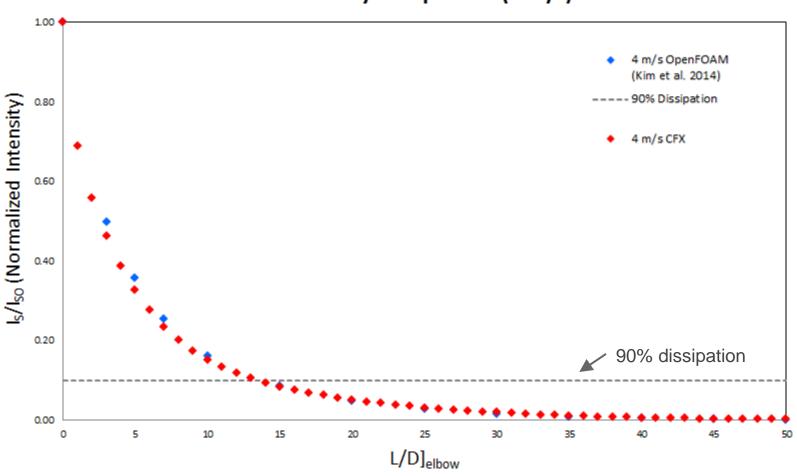
#### Swirl Intensity dissipates 90% by 15D after an elbow in CFX simulations.

#### Swirl Intensity Comparsion (4 m/s)

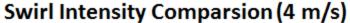


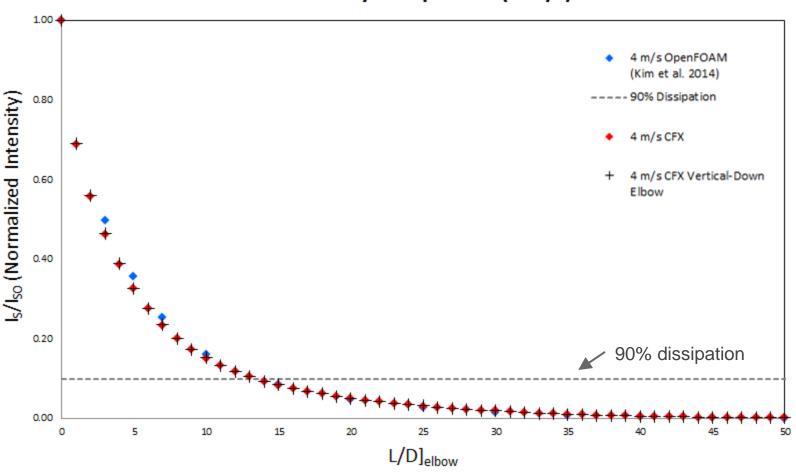
#### Swirl Intensity dissipates 90% by 15D after an elbow in CFX simulations.





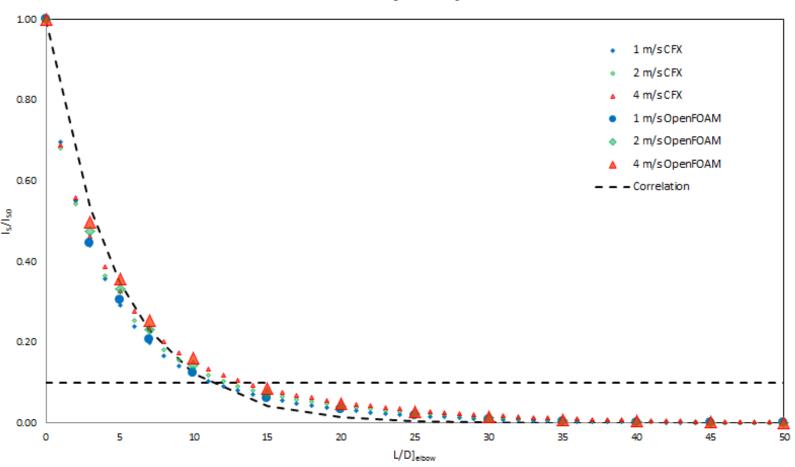
#### Swirl Intensity dissipation is independent of elbow orientation.



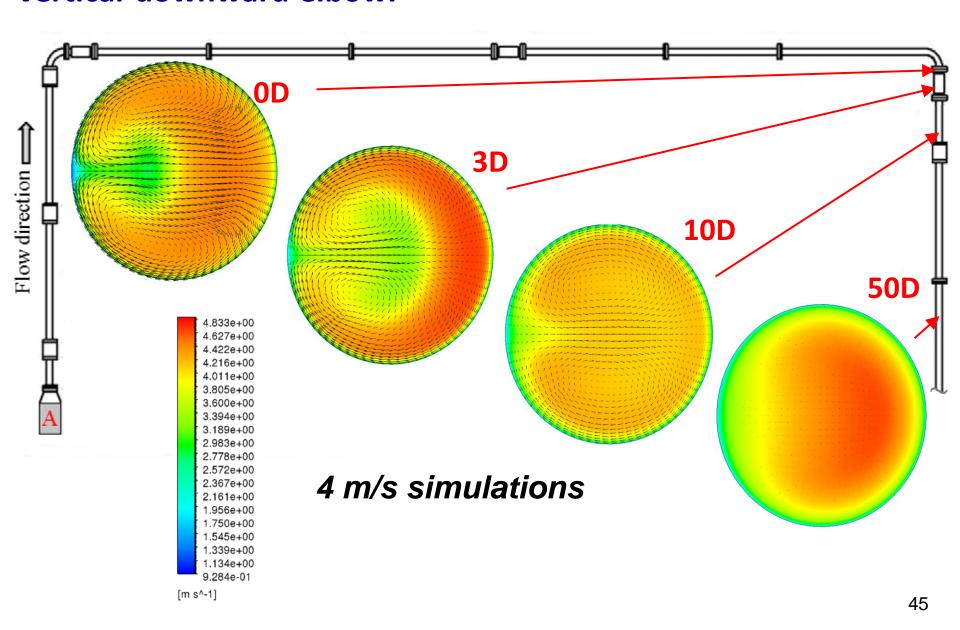


# The CFX simulations match the Swirl Intensity decay of OpenFOAM results.

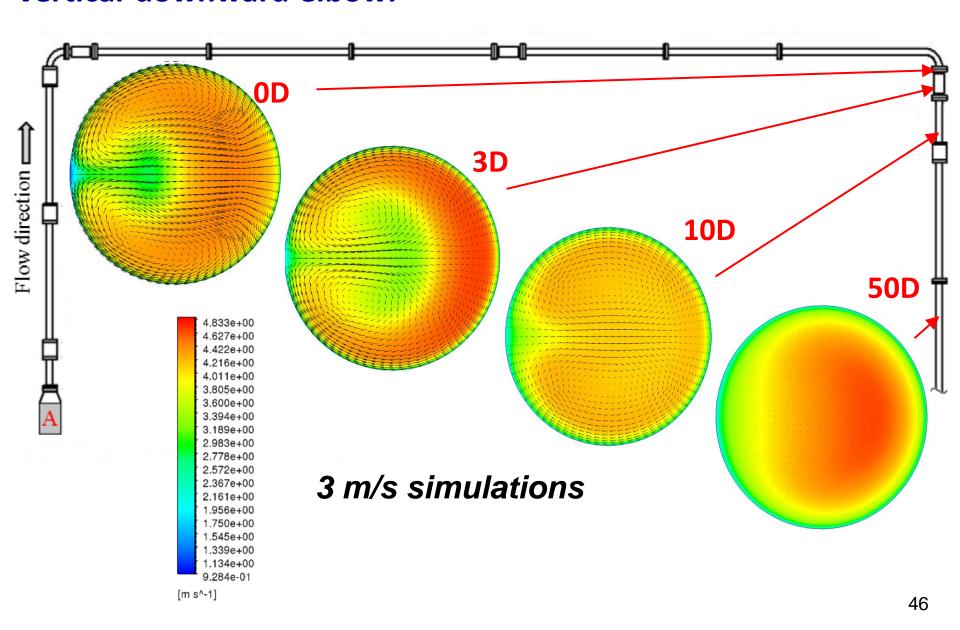




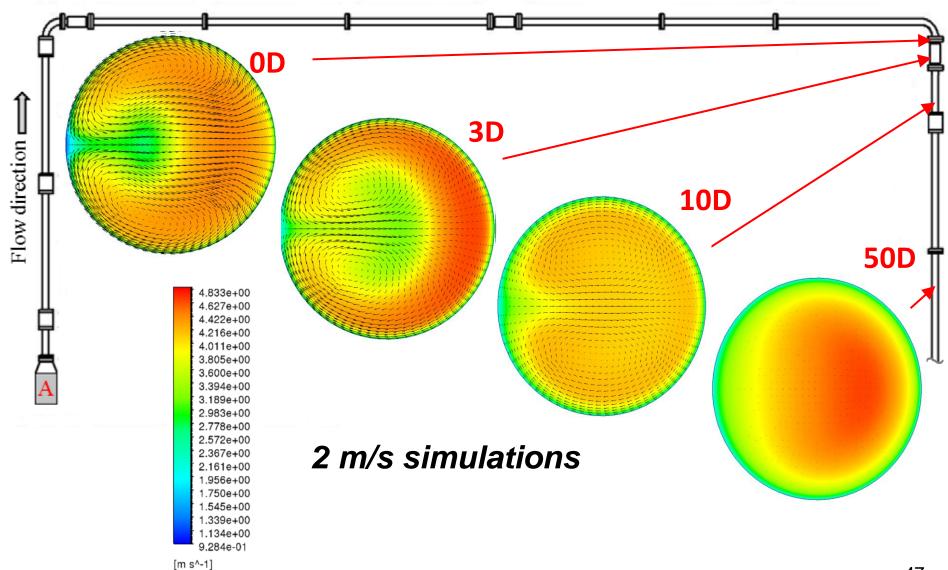
#### CFD models were analyzed at 0D, 3D, 10D, and 50D after the vertical-downward elbow.



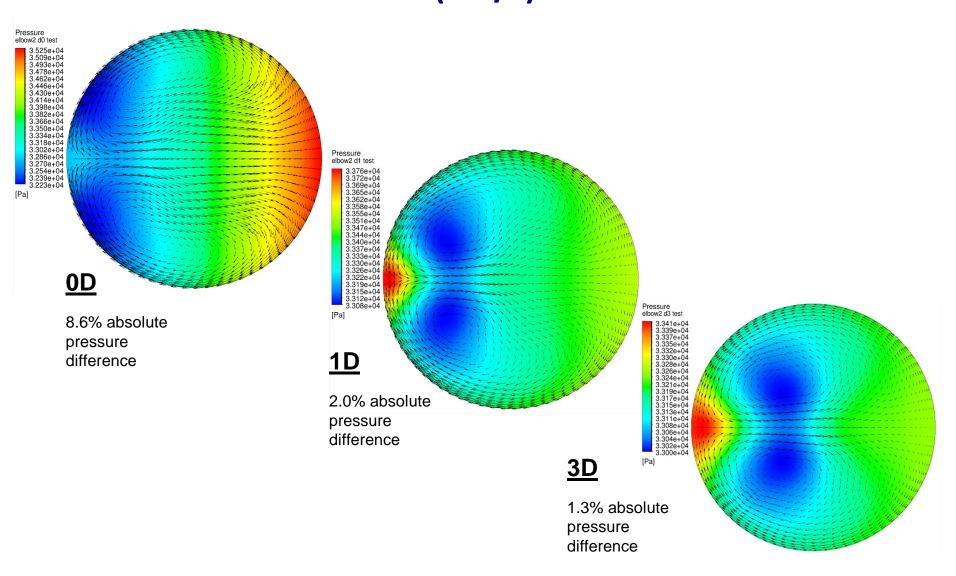
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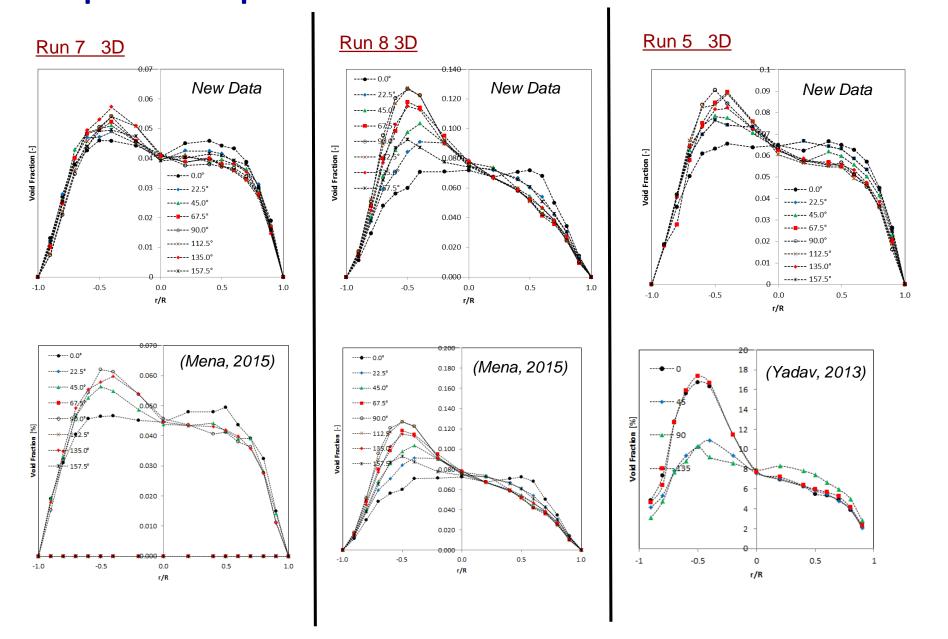
# Pressure distribution changes at 0D, 1D, and 3D after the vertical-downward elbow (4m/s)



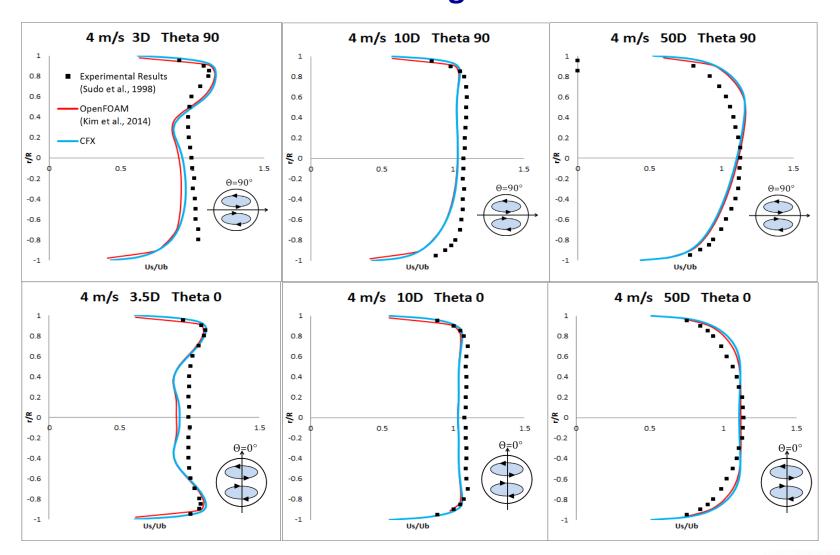
# The area average void fraction and elbow strength of our data is comparable to previous research.

	Current	Mena	% Difference
RUN 7			
<α> [-]	0.047	0.066	28.8%
σ [-]	0.4821	0.5638	14.5%
RUN 5			
<α> [-]	0.031	0.034	8.82
σ [-]	0.2464	0.2422	1.73
RUN 8			
<α> [-]	0.046	0.05	8.00
σ [-]	0.2642	0.2585	2.21

The area average void fraction and elbow strength of our data is comparable to previous research.

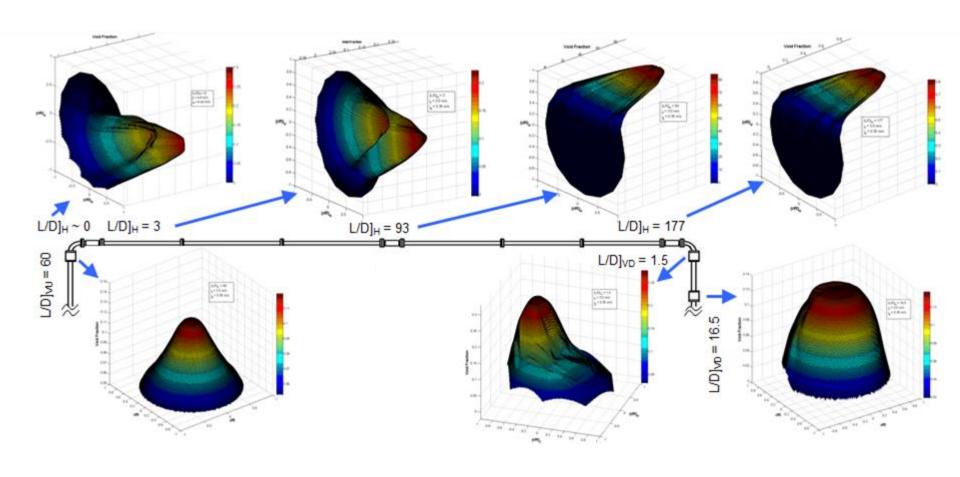


# OpenFoam simulations from Kim et al. (2014) agree closely with CFX results over entire elbow length.



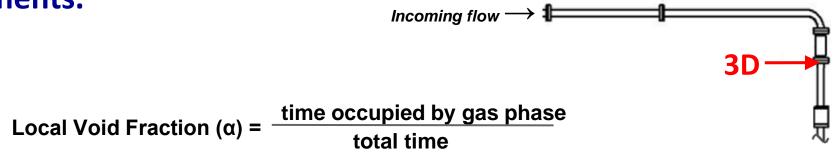


# Surface contours created from previous studies help better understand flow regime of the facility

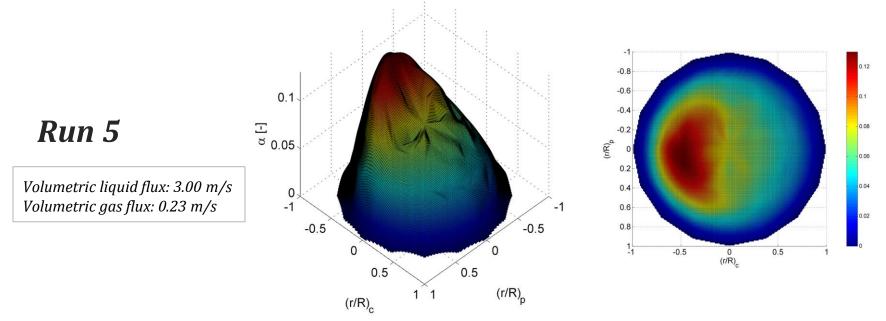




# Surface plots and Contour plots show void fractions from experiments.

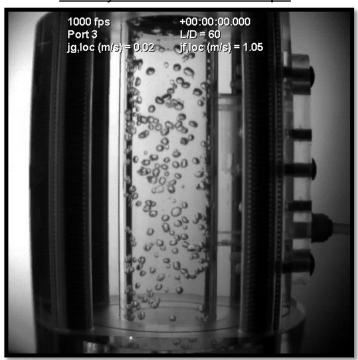


Repeat experiments, such as Run 5, confirm consistency with previous data.



#### The objective of this research is to investigate two-phase flow after a vertical-downward elbow.

**Bubbly Flow In Vertical Pipe** 



**Bubbly Flow In Vertical-Upward Elbow** 



Flow rates and geometry dramatically change flow characteristics